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Talyrond, [1,2],

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24642-81 [3]

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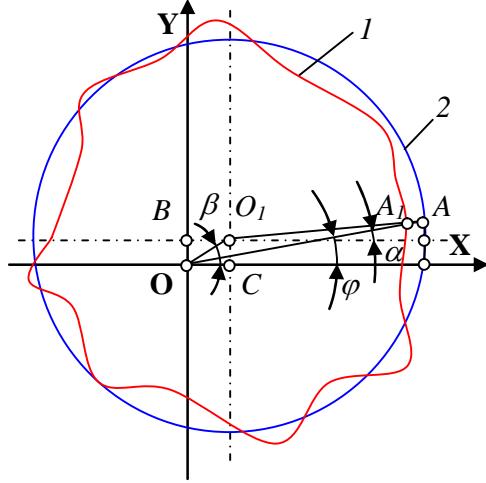
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$$\begin{cases} OA \cdot \cos \varphi = OO_1 \cdot \cos \beta + O_1 A \cdot \cos \alpha \\ OA \cdot \sin \varphi = OO_1 \cdot \sin \beta + O_1 A \cdot \sin \alpha \end{cases} \quad (1)$$

$$\cos \alpha = \frac{OA \cdot \cos \varphi - OO_1 \cdot \cos \beta}{O_1 A}, \quad (2)$$

$$\sin^2 \alpha = \frac{O_1 A^2 - OA^2 \cdot \cos^2 \varphi + 2 \cdot OA \cdot OO_1 \cos \varphi \cdot \cos \beta - OO_1^2 \cdot \cos^2 \beta}{O_1 A^2}. \quad (3)$$

(1),

$$(OA \cdot \sin \varphi - OO_1 \cdot \sin \beta)^2 = O_1 A^2 \cdot \sin^2 \alpha$$

OA

$$OA^2 - a \cdot OA + b = 0, \quad (4)$$

$$a = 2 \cdot OO_1 \cdot (\sin \varphi \cdot \sin \beta + \cos \varphi \cdot \cos \beta), \quad b = OO_1^2 - O_1 A^2.$$

(4)

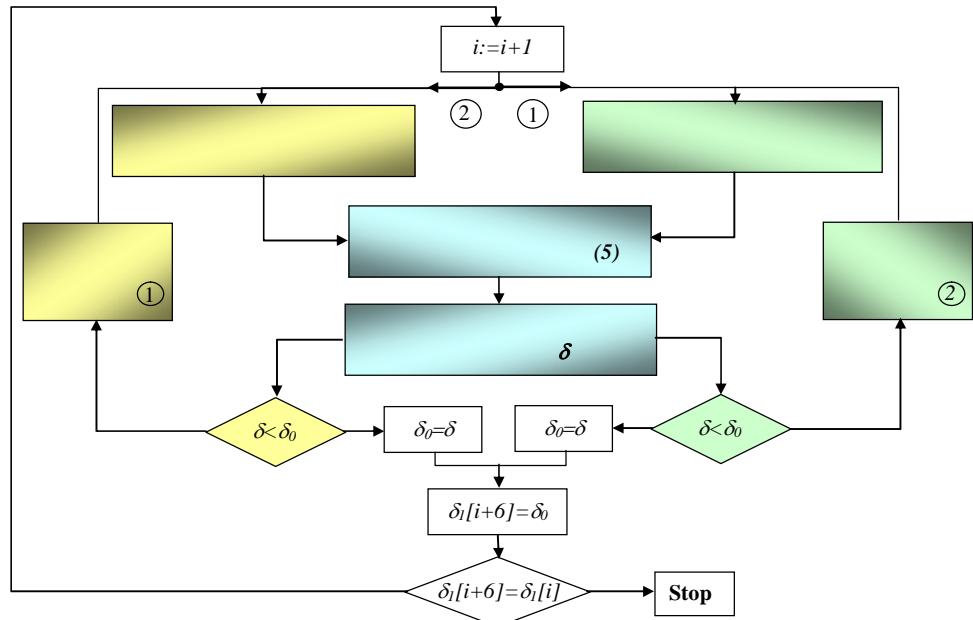
OA

φ

$$(OA)_{1,2} = OO_1 (\sin \varphi \sin \beta + \cos \varphi \cos \beta) \pm \sqrt{(OO_1 (\sin \varphi \sin \beta + \cos \varphi \cos \beta))^2 - OO_1^2 + O_1 A^2}. \quad (5)$$

($i = I$) β),

, .2.



.2.

$(i=I)$

β

(5)

δ

, $\delta < \delta_0$, $\delta_0 -$

.2 - .1

$\delta < \delta_0$, .1

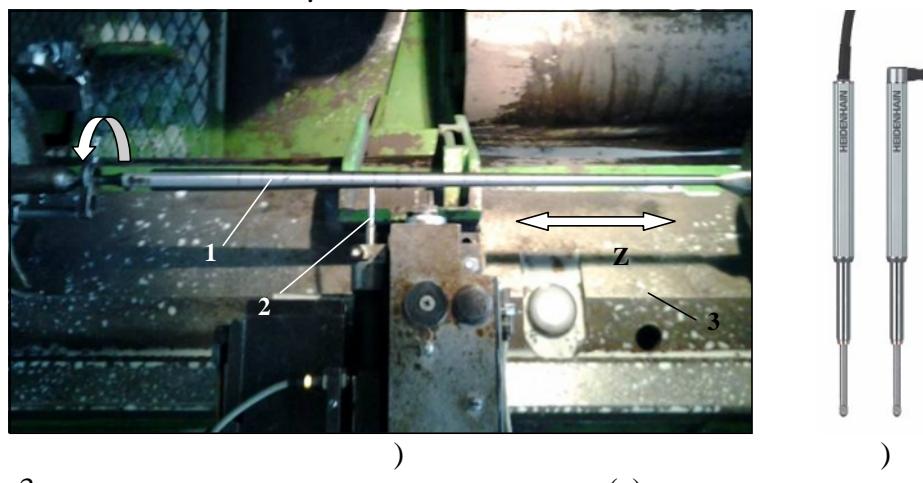
.2. $\delta_1[i+6] = \delta_1[i]$, .1

4.

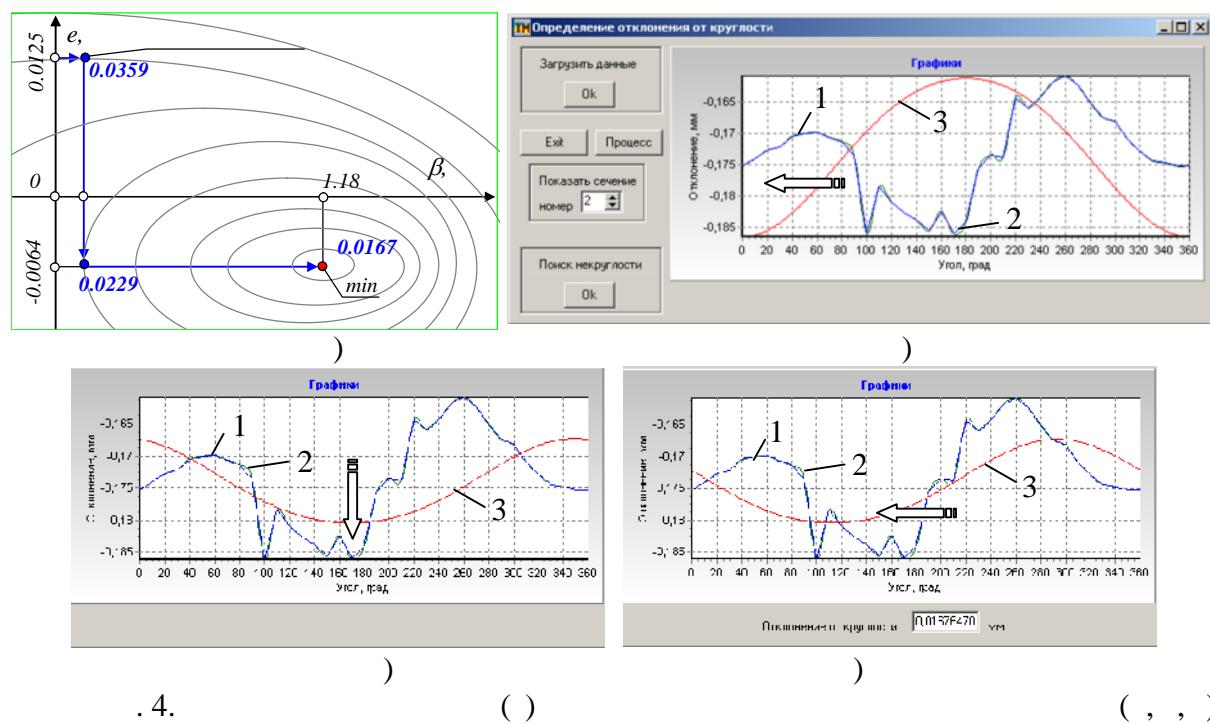
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 10^0

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3. Heidenhain ()



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www.bru.mogilev.by/students
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4. 24642-81. .118-162.
www.heidenhain.de HEIDENHAIN //

Petrakov Y.V.

**CONTROL OF CIRCULARITY DEVIATION
AT GRINDING ON CNC MACHINE-TOOLS**

It is suggested to measure the rejections of form of details, in particular, deviation from a roundness, directly on a machine-tool with CHPU at implementation of operation of polishing of important details. The algorithm of calculation of circularity deviation is developed based on the analysis of points array of radial run-out of the real shape in controlled section of detail. A control method and algorithm were approved by determination of circularity deviation of working surface of finger for cold rolling of pipes on the modernized CNC grinding machine-tools.

Keywords: Circularity deviation, grinding on a CNC machine-tools.

30.05.2013 .