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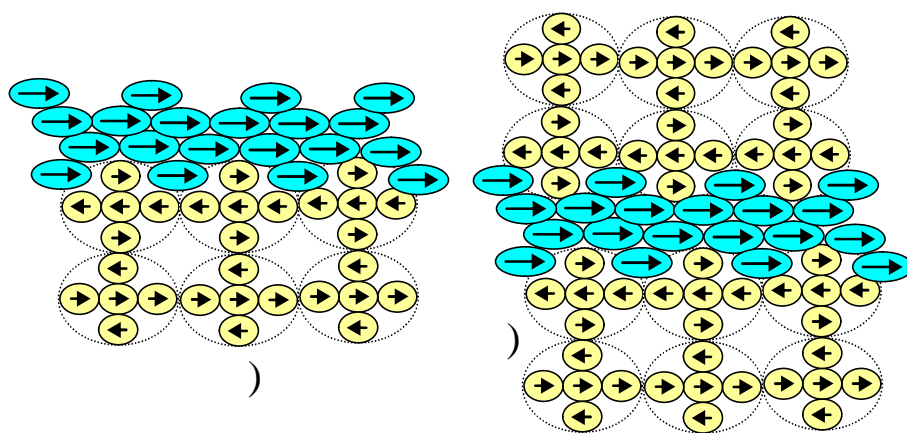
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0,471 Å.

$7,33 \cdot 10^{-30}$. .

[9]

$5,37 \cdot 10^{-30}$. .

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[10],

[12].

$$E = \begin{cases} -\frac{2E R_0^6}{r^6} + \frac{E R_0^{12}}{r^{12}}, & r \leq R_0; \\ \sum_{i=1}^3 N_i \kappa_i^2 \left[\sum_{k=0}^3 \sum_{l=0}^3 Z_{a,k}^* Z_{b,l}^* \int_{(a)} \int_{(b)} \rho_{e,a}(\varepsilon_k) \rho_{e,l}(\varepsilon_l) \left(\frac{H_{1,1} + H_{1,2}}{1+S} \right) d\varepsilon_k d\varepsilon_l \right] & r > R_0. \end{cases} \quad (1)$$

$$\begin{aligned} & R_0 - \dots; N_i - \dots; \\ & \dots; Z_{a,k}^*, Z_{b,l}^* - \dots; \\ & \dots; \rho_{e,a}(\varepsilon_k), \rho_{e,b}(\varepsilon_l) - \dots; \\ & \dots; S - \dots, \dots \end{aligned}$$

$$E = [(1-P_1)P_2 + (1-P_2)P_1]S(1-S) \frac{e^2}{4\pi\varepsilon_0 R_0}. \quad (2)$$

$$1 \quad 2 - \dots, S - \dots$$

$$E = P_1 P_2 (1-S)^2 \frac{e^2}{4\pi\varepsilon_0} \left[\frac{Z_1^*}{r_1} + \frac{Z_2^*}{r_2} \right]. \quad (3)$$

$$E_{e-d} = 2P_1(1-P_2)(1-S)S \frac{ep_{,2}}{4\pi\varepsilon_0 R_0^2} - (1-P_1)P_2(1-S)S \frac{e(p_{,1} - p_{,2})}{4\pi\varepsilon_0 R_0^2}, \quad (4)$$

$$\begin{aligned} & \cdot,1 \quad \cdot,2 \quad - \\ & , \quad (1 - S) \quad (4) \end{aligned}$$

- .

$$\begin{aligned} & [6]: \\ E_{-} &= \frac{p_{,1} \cdot,2 \varphi(\alpha_i, N_i)}{4\pi\epsilon_0 R_0^3}. \end{aligned} \quad (5)$$

R_0 -

; $\varphi(\alpha_i, N_i)$ -

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XZ YZ .

$$E_{-} (1) = \cdot,0 + k \cdot$$

$$(2,3) = \cdot,0 + 2k \cdot \quad (6)$$

$$E_{-} = E_{-0} + 3k \cdot T \cdot \quad (7)$$

[9,10].

(0,68 - 0,74).

0,44 - 0,47 [13].

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(9).

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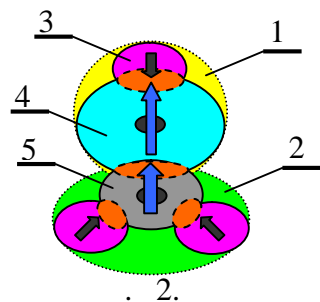
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$$W = \int_0^E f(E, T) dE \quad (10)$$

.3 —

[9,10].



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$$= \frac{U(r) - U(r_0)}{r_0 S^2}, \quad (11)$$

$U(r)$, $U(r_0)$ –
 r
 r_0 ; S – ; –

$e=0,005$, $5,5 \cdot 10^{10}$, $1,7 \cdot 10^{11}$, $1,0 \cdot 10^{11}$.

$4,16 \cdot 10^{10}$ [14].



0,254 , $6.5 \cdot 10^{10}$.

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1,85

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i i c i (« ») – . 2011. - . 31. - . 100-108.

2.

3. // XIX 17-22 2012 . 3- . – : , 2012. - . 1. - . 195 – 197.

4. // IV 11-13 2007. – : , 2007. - . 229 - 223.

5. / . . . , . . .
 , // , 2004. - 1. - . 48 - 53.
6. Cu – Fe / .
 , . . . , . . . , . // , 2005. - 1. - . 36 –
39. 7. / . . .
 , . . . // , 2012. - 2. . 26. - . 259-264.
8. / . . . , . . . //
 , 2010. - 1. - . 5-13.
9. / . . . , . . .
 // . i i i i i i / i . . .
 . . . – i : i - i i i . . . i ,
 2009. . 315-320.
10. / . . . // . :
 , 2004. – 398 .
11. . . . / . . . // . :
 . 2008. – 406 .
12. . . . / . . . // . : , 1965. – 426 .
13. . . . // . : « . - 2010. – 75 .
14. . . . // . : . - 1991. – 160 .
15. . . . / . . . // (05 23 05).
 . - 2008.

L.I. Grechikhin, E.D. Podlozny
CLOSE-PACKED STATE AND ITS ROLE IN
THE HARDENING OF CONSTRUCTION
MATERIALS

It is shown that the close-packed state increases the binding energy of the binary interaction between the different materials in composite structures, and using the example of high-strength concrete demonstrated the effectiveness of the binder in the form of a close-packed state.

Keywords: construction materials close-packed state, Young's modulus, a binary relation, the mechanical properties

14.06.2013 .