

621.793.02

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42CrMo4.

1,5

1.

[1], [2], [3],

[4], [5].

1)
2)
3)

4) ;
 5)

2.

Co6% PVD- , WC-
 TiAlN 4E- ATI Stellram [6],

.. Sandvik Coromant DCLNR3232P-16
 , =6°, =6°.
 =45°.
 42CrMo4 (38)
 850° 180
 600° 240 , 38 HRC.
 1.
 2500 / 2. , , , , , ,
 . , , , , , ,
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 ,

1. 42CrMo4								
C%	Si% max	Mn%	P% max	S% max	Cr%	Mo%	Fe	
0,38-0,45	0,40	0,60-0,90	0,025	0,035	0,90-1,20	0,15-0,30		

- ABAQUS
 Explicit 6.10 ,
 , PVD- ,
 ,
 ,
 ,
 ,

H.Ernault Somua 450 NCS ,
 2.

2.

	/ ,	, /	,
v200s03t3	200	0,3	3
v150s03t3	150	0,3	3
v100s03t3	100	0,3	3
v150s01t3	150	0,1	3

WC-Co6%
 PVD- TiAlN 4E- ATI Stellram

(
,
t):

$$T = e^{k + x \cdot \ln(\sigma) + y \cdot \ln(\tau) + z \cdot \ln(t)}, \quad (1)$$

k, x, y, z -

42CrMo4.

$$\begin{cases} \ln(T_{v200s03t3}) = k + x \cdot \ln(\sigma_{v200s03t3}) + y \cdot \ln(\tau_{v200s03t3}) + z \cdot \ln(t_{v200s03t3}) \\ \ln(T_{v150s03t3}) = k + x \cdot \ln(\sigma_{v150s03t3}) + y \cdot \ln(\tau_{v150s03t3}) + z \cdot \ln(t_{v150s03t3}) \\ \ln(T_{v100s03t3}) = k + x \cdot \ln(\sigma_{v100s03t3}) + y \cdot \ln(\tau_{v100s03t3}) + z \cdot \ln(t_{v100s03t3}) \\ \ln(T_{v150s01t3}) = k + x \cdot \ln(\sigma_{v150s01t3}) + y \cdot \ln(\tau_{v150s01t3}) + z \cdot \ln(t_{v150s01t3}) \end{cases}; \quad (2)$$

3.

3.

				T,
	,	,	o	t,
v200s03t3	2345	85	655	260
v150s03t3	1125	40	620	740
v100s03t3	3150	35	570	780
v150s01t3	1535	50	445	2200

$$, k=39; x=-0,42; y=-0,67; z=-4,2,$$

:

$$T = e^{39 - 0,42 \cdot \ln(\sigma) - 0,67 \cdot \ln(\tau) - 4,2 \cdot \ln(t)}, \quad (3)$$

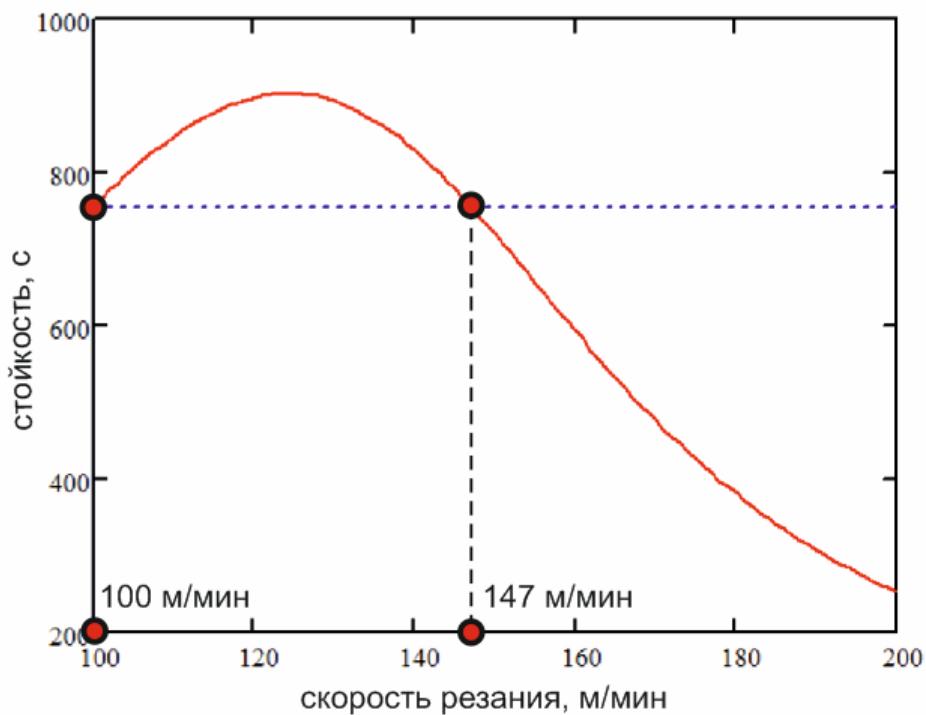
200 / .
0,3 /
3
-
,
)
42CrMo4 (. 1).
:

$$K_p = \frac{1}{t_o}, \quad (5)$$

t_o – время, необходимое для

$$t_o = \frac{\pi \cdot D \cdot L}{1000 \cdot v \cdot s}, \quad (6)$$

D – диаметр, мм; v – скорость резания, м/мин; L – длина обработки, м; s – коэффициент, зависящий от материала и условий обработки.



1. 42CrMo4

42CrMo4
1, 100 147 /
1,5 .

3.

1,5

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IMPROVING TECHNOLOGICAL PERFORMANCE OF TURNING WITHOUT REDUCTION OF STRENGTH OF CUTTING PLATE

The presented method takes into account the physical and mechanical processes in the cutting zone, and can significantly reduce the amount of experimental studies to determine the cutting process to enhance performance on an example of turning of hardened alloy steel 42CrMo4. Through the presented model of the strength of cutting plate is determined dependence of the strength of cutting plate and cutting speed, which allowed to improve the technological performance by 1.5 times without reduction of strength of cutting plate.

Keywords: technological performance, turning, physical and mechanical processes, strength, cutting conditions.